

# MAXIMA 7

## Zinc Coated Anchor Stud (G5.8)



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### Bonded Anchor in Glass Capsule

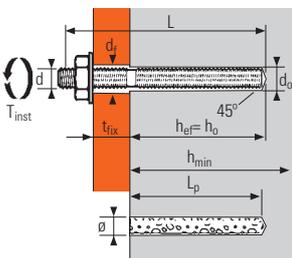
Performance				Material	Installation							

### Technical Data

MAXIMA 7	Anchor depth (mm)	Max thick of fixture (mm)	Drill depth (mm)	Min thick of base material (mm)	Ø Thread (mm)	Ø Drill bit (mm)	Total anchor length (mm)	Max tighten torque (Nm)	Chemset stud code	Ramset power tool code	Drill bit type-size
	$h_{ef}$	$t_{fix}$	$h_o$	$h_{min}$	$d$	$d_o$	$L$	$T_{inst}$			
MAXIMA M8	80	15	80	120	8	10	110	10	CS08110	DD527	R3 PLUS-10
MAXIMA M10	90	20	90	130	10	12	130	20	CS10130	DD527	R3 PLUS-12
MAXIMA M12	110	25	110	160	12	14	160	30	CS12160	DD527	R3 PLUS-14
MAXIMA M16	125	35	125	175	16	18	190	60	CS16190	DD543	R3 PLUS-18
MAXIMA M20	170	65	170	220	20	25	260	120	CS20260	DD565	R3 MAX-25
MAXIMA M24	210	63	210	270	24	28	300	200	CS24300	DD565	R3 MAX-28
MAXIMA M30	280	70	280	340	30	35	380	400	CS30380	DD565	R3 MAX-35



ETA Option 7  
n° 03/0007



### MATERIAL

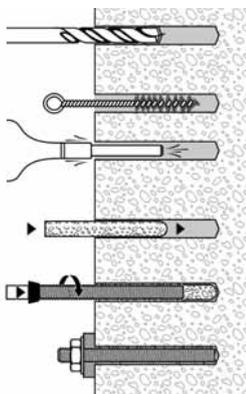
Stud:  
Grade 5.8

Hexagonal nut:  
Grade 6 or 8

Washer:  
Steel

Coating:  
Zinc coated (5µm)

### INSTALLATION



### Anchor Mechanical Properties

CARBON STEEL Grade 5.8	M8	M10	M12	M16	M20	M24	M30
$f_{uk}$ (N/mm <sup>2</sup> ) Min. tensile strength	540	540	540	520	520	520	520
$f_{yk}$ (N/mm <sup>2</sup> ) Yield strength	430	430	430	420	420	420	420
$A_s$ (mm <sup>2</sup> ) Stressed cross-section	36.6	58.0	84.3	157.0	245.0	353.0	522.8
$W_{el}$ (mm <sup>3</sup> ) Elastic section modulus	31.2	62.3	109.2	277.5	540.9	935.5	1,686.0
$M^0_{Rk,s}$ (Nm) Characteristic bending moment	20.2	40.4	70.7	173.1	301.1	520.2	1,052.1
$M$ (Nm) Recommended bending moment	16.2	32.3	56.6	138.5	240.8	416.2	841.7

### Setting Time before applying load

Ambient temperature (°C)	Dry concrete	Wet concrete
	Waiting time before apply load	Waiting time before apply load
$T \geq 20^\circ\text{C}$	20 min	40 min
$10^\circ\text{C} < T < 20^\circ\text{C}$	30 min	60 min
$0^\circ\text{C} < T < 10^\circ\text{C}$	1 hour	2 hours
$-5^\circ\text{C} < T < 0^\circ\text{C}$	5 hours	10 hours

### Chemical Resistance of the MAXIMA Anchor

Chemical substances	Concentration (%)	Resistance	Chemical substances	Concentration (%)	Resistance
Nitric Acid	< 20	1	Carbon monoxide	100	1
Phosphoric acid	< 10	1	Caustic potash	100	1
Sulphuric acid	$\leq 30$	1	Nitric Acid	20 - 70	2
Ethyl alcohol	$\leq 15$	1	Heptane	100	2
Beer	100	1	Hexane	100	2
Carbon dioxide	100	1	Methanol	$\leq 15$	2
Hydrogen fluoride	$\leq 20$	1	Perchloroethylene	100	2
Ammonia	100	1	Hydrogen peroxide	$\leq 40$	2
Ethylene glycol	100	1	Sulphurous acid	100	2
Washing powder	100	1	Engine petrol w/o benzene	100	2
Cement in suspension saturated solution		1			

1 = High resistance (Anchors could be submerged in these materials)

2 = Medium resistance (Anchors could be temporary submerged due to splash or spill)

# MAXIMA 7

## Zinc Coated Anchor Stud (G5.8)



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### Ultimate Loads ( $N_{Ru,m}$ , $V_{Ru,m}$ ) / Characteristic Loads ( $N_{Rk}$ , $V_{Rk}$ ) in kN

#### TENSILE @ Concrete strength 30 N/mm<sup>2</sup>

Anchor size	M8	M10	M12	M16	M20	M24	M30
$h_{ef}$ (mm)	80	90	110	125	170	210	280
$N_{Ru,m}$ (kN)	21.3	33.8	49.2	88.2	167.8	231.6	327.5
$N_{Rk}$ (kN)	19.8	31.3	45.5	81.6	125.8	173.7	270.7

#### SHEAR @ Concrete strength 30 N/mm<sup>2</sup>

Anchor size	M8	M10	M12	M16	M20	M24	M30
$V_{Ru,m}$ (kN)	12.8	20.3	29.5	52.9	82.6	118.9	176.2
$V_{Rk}$ (kN)	11.9	18.8	27.3	49.0	76.4	110.1	163.1

### Design Loads ( $N_{Rd}$ , $V_{Rd}$ ) for one anchor without edge or spacing influence in kN

$$N_{Rd} = \frac{N_{Rk}}{\gamma_{Mc,N}}$$

$$V_{Rd} = \frac{V_{Rk}}{\gamma_{Ms,V}}$$

#### TENSILE @ Concrete strength 30 N/mm<sup>2</sup>

Anchor size	M8	M10	M12	M16	M20	M24	M30
$h_{ef}$ (mm)	80	90	110	125	170	210	280
$N_{Rd}$ (kN)	13.2	20.9	30.3	54.4	69.9	96.5	150.4

$$\gamma_{Mc,N} = 1.8$$

$$\gamma_{Ms,N} = 1.5 \text{ (steel failure)}$$

#### SHEAR @ Concrete strength 30 N/mm<sup>2</sup>

Anchor size	M8	M10	M12	M16	M20	M24	M30
$V_{Rd}$ (kN)	9.5	15.0	21.9	39.2	61.2	88.1	130.5

$$\gamma_{Ms,V} = 1.25$$

### Recommended Loads ( $N_{rec}$ , $V_{rec}$ ) for one anchor without edge or spacing influence in kN

$$N_{rec} = \frac{N_{Rk}}{\gamma_{Mc,N} \cdot \gamma_F}$$

$$V_{rec} = \frac{V_{Rk}}{\gamma_{Ms,V} \cdot \gamma_F}$$

#### TENSILE @ Concrete strength 30 N/mm<sup>2</sup>

Anchor size	M8	M10	M12	M16	M20	M24	M30
$h_{ef}$ (mm)	80	90	110	125	170	210	280
$N_{rec}$ (kN)	9.4	14.9	21.7	38.9	49.9	68.9	107.4

$$\gamma_F = 1.4$$

$$\gamma_{Mc,N} = 1.8$$

$$\gamma_{Ms,N} = 1.5 \text{ (steel failure)}$$

#### SHEAR @ Concrete strength 30 N/mm<sup>2</sup>

Anchor size	M8	M10	M12	M16	M20	M24	M30
$V_{rec}$ (kN)	6.8	10.7	15.6	28.0	43.7	62.9	93.2

$$\gamma_F = 1.4$$

$$\gamma_{Ms,V} = 1.25$$

steel failure

# MAXIMA 7

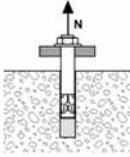
## Zinc Coated Anchor Stud (G5.8)



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### CC-Method

#### TENSILE in kN



Pull-out resistance  
Concrete strength 30 N/mm<sup>2</sup>

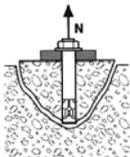
$$N_{Rd,p} = N^0_{Rd,p} \cdot f_B \cdot f_T$$

N <sup>0</sup> <sub>Rd,p</sub>		Design resistance in dry and wet concrete						
Anchor size		M8	M10	M12	M16	M20	M24	M30
h <sub>ef</sub> (mm)		80	90	110	125	170	210	280
N <sup>0</sup> <sub>Rd,p</sub> (kN)		11.9	20.2	30.8	42.7	69.9	96.5	150.4

N <sup>0</sup> <sub>Rd,p</sub>		Design resistance in flooded concrete						
Anchor size		M8	M10	M12	M16	M20	M24	M30
N <sup>0</sup> <sub>Rd,p</sub> (kN)		8.5	14.4	22.0	30.5	49.9	68.9	107.4

$$\gamma_{Mc,N} = 1.8$$

$$\gamma_{Mc,N} = 2.52 \text{ (flooded)}$$



Concrete cone resistance for dry (1), wet (2) and flooded (3) concrete

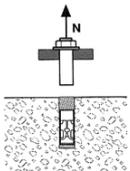
$$N_{Rd,c} = N^0_{Rd,c} \cdot f_B \cdot f_T \cdot \Psi_s \cdot \Psi_{c,N}$$

N <sup>0</sup> <sub>Rd,p</sub>		Design resistance in dry and wet concrete						
Anchor size		M8	M10	M12	M16	M20	M24	M30
h <sub>ef</sub> (mm)		80	90	110	125	170	210	280
N <sup>0</sup> <sub>Rd,c</sub> (kN)		26.3	31.4	42.5	51.4	81.6	112.0	172.5

N <sup>0</sup> <sub>Rd,p</sub>		Design resistance in flooded concrete						
Anchor size		M8	M10	M12	M16	M20	M24	M30
N <sup>0</sup> <sub>Rd,c</sub> (kN)		15.7	18.7	25.3	30.6	48.6	66.7	102.6

$$\gamma_{Mc,N} = 1.5$$

$$\gamma_{Mc,N} = 2.52 \text{ (flooded)}$$



Steel resistance

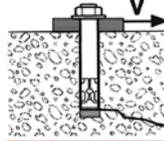
N <sub>Rd,s</sub>		Steel design tensile resistance						
Anchor size		M8	M10	M12	M16	M20	M24	M30
N <sub>Rd,s</sub> (kN)		13.2	20.9	30.3	54.4	84.9	122.4	181.2

$$\gamma_{Ms,N} = 1.5$$

$$N_{Rd} = \min(N_{Rd,p}; N_{Rd,c}; N_{Rd,s})$$

$$\beta N = N_{Sd} / N_{Rd} \leq 1$$

#### SHEAR in kN

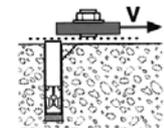


Concrete edge resistance  
Concrete strength 30 N/mm<sup>2</sup>

$$V_{Rd,c} = V^0_{Rd,c} \cdot f_B \cdot f_{\beta,V} \cdot \Psi_{s-c,V}$$

V <sup>0</sup> <sub>Rd,c</sub>		Design concrete edge resistance at a minimum edge distance (c <sub>min</sub> )						
Anchor size		M8	M10	M12	M16	M20	M24	M30
h <sub>ef</sub> (mm)		80	90	110	125	170	210	280
c <sub>min</sub>		40	45	55	65	85	105	140
s <sub>min</sub>		40	45	55	65	85	105	140
V <sup>0</sup> <sub>Rd,c</sub> (kN)		2.8	3.6	5.3	7.5	13.3	19.7	34.3

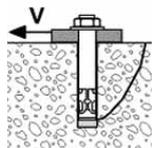
$$\gamma_{Mc,V} = 1.5$$



Steel resistance

V <sub>Rd,s</sub>		Steel design shear resistance						
Anchor size		M8	M10	M12	M16	M20	M24	M30
V <sub>Rd,s</sub> (kN)		9.5	15.0	21.9	39.2	61.2	88.1	130.5

$$\gamma_{Ms,V} = 1.25$$



Concrete pry-out failure  
Concrete Strength 30 N/mm<sup>2</sup>

$$V_{Rd,cp} = V^0_{Rd,cp} \cdot f_B \cdot \Psi_s \cdot \Psi_{c,N}$$

V <sup>0</sup> <sub>Rd,cp</sub>		Design pry-out resistance						
Anchor size		M8	M10	M12	M16	M20	M24	M30
V <sup>0</sup> <sub>Rd,cp</sub> (kN)		23.5	36.7	58.6	88.0	110.0	168.7	205.4

$$\gamma_{Mc,V} = 1.5$$

- (1) for dry hole,  $\gamma_{Mc} = 2.16$  where brush is not use to clean hole
- (2) The concrete in the area of the anchorage is water saturated.
- (3) The concrete is wet, and the is full of water. The resin can be injected without remove water.

$$V_{Rd} = \min(V_{Rd,c}; V_{Rd,s}; V_{Rd,cp})$$

$$\beta V = V_{Sd} / V_{Rd} \leq 1$$

$$\beta N + \beta V \leq 1.2$$

#### f<sub>B</sub> INFLUENCE OF CONCRETE

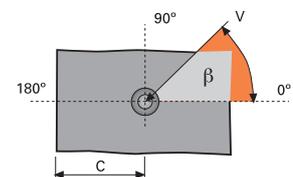
Concrete Grade	f <sub>B</sub>	Concrete Grade	f <sub>B</sub>
C16/20	0.81	C35/45	1.21
C20/25	0.90	C40/50	1.28
C25/30	1.00	C45/55	1.34
C30/37	1.10	C50/60	1.40

#### f<sub>T</sub> INFLUENCE OF EMBEDMENT DEPTH

$$f_T = \frac{h_{act}}{h_{ef}} \quad \text{where: } h_{ef} \leq h_{act} \leq 2h_{ef}$$

#### f<sub>β,V</sub> INFLUENCE OF SHEAR LOADING DIRECTION

Angle β [°]	f <sub>β,V</sub>
0~50	1.0
60	1.1
70	1.2
80	1.5
90~180	2.0



# MAXIMA 7

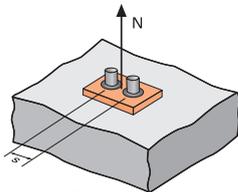
## Zinc Coated Anchor Stud (G5.8)



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### CC-Method

#### $\Psi_s$ INFLUENCE OF SPACING FOR CONCRETE CONE RESISTANCE IN TENSILE LOAD



$$\Psi_s = 0.5 + \frac{s}{4h_{ef}}$$

$$s_{min} < s < s_{cr,N}$$

$$s_{min} = 0.5h_{ef}$$

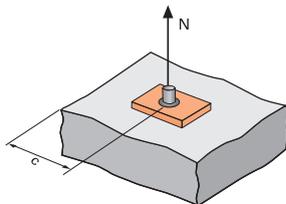
$$s_{cr,N} = 2h_{ef}$$

$\Psi_s$  must be used for each spacing influenced the anchors group

Spacing, s	Reduction Factor $\Psi_s$ Non-cracked concrete			
	M8	M10	M12	M16
40	0.63			
45	0.64	0.63		
55	0.67	0.65	0.63	
65	0.70	0.68	0.65	0.63
85	0.77	0.74	0.69	0.67
105	0.83	0.79	0.74	0.71
140	0.94	0.89	0.82	0.78
160	1.00	0.94	0.86	0.82
180		1.00	0.91	0.86
220			1.00	0.94
250				1.00

Spacing, s	Reduction Factor $\Psi_s$ Non-cracked concrete		
	M20	M24	M30
85	0.63		
105	0.65	0.63	
140	0.71	0.67	0.63
160	0.74	0.69	0.64
180	0.76	0.71	0.66
220	0.82	0.76	0.70
250	0.87	0.80	0.72
300	0.94	0.86	0.77
340	1.00	0.90	0.80
370		0.94	0.83
450		1.00	0.90
560			1.00

#### $\Psi_{c,N}$ INFLUENCE OF EDGE FOR CONCRETE CONE RESISTANCE IN TENSILE LOAD



$$\Psi_{c,N} = 0.275 + 0.725 \cdot \frac{c}{h_{ef}}$$

$$c_{min} < c < c_{cr,N}$$

$$c_{min} = 0.5h_{ef}$$

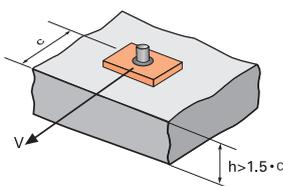
$$c_{cr,N} = h_{ef}$$

$\Psi_{c,N}$  must be used for each distance influenced the anchors group

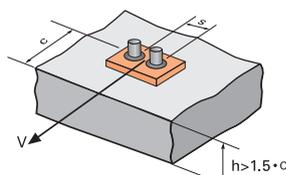
Edge, c	Reduction Factor $\Psi_{c,N}$ Non-cracked concrete			
	M8	M10	M12	M16
40	0.63			
45	0.68	0.63		
55	0.77	0.71	0.63	
65	0.86	0.79	0.70	0.66
80	1.00	0.91	0.80	0.73
90		1.00	0.86	0.79
110			1.00	0.91
125				1.00

Edge, c	Reduction Factor $\Psi_{c,N}$ Non-cracked concrete		
	M20	M24	M30
85	0.63		
105	0.72	0.63	
120	0.78	0.68	
140	0.87	0.75	0.63
170	1.00	0.86	0.71
210		1.00	0.81
250			0.92
280			1.00

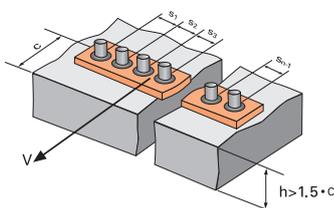
#### $\Psi_{s-c,V}$ INFLUENCED OF SPACING AND EDGE DISTANCE FOR CONCRETE EDGE RESISTANCE IN SHEAR LOAD



$$\Psi_{s-c,V} = \frac{c}{c_{min}} \cdot \sqrt{\frac{c}{c_{min}}}$$



$$\Psi_{s-c,V} = \frac{3c + s}{6c_{min}} \cdot \sqrt{\frac{c}{c_{min}}}$$



##### FOR SINGLE ANCHOR FASTENING

Reduction Factor  $\Psi_{s-c,V}$

Non-cracked concrete

$\frac{c}{c_{min}}$	1.0	1.2	1.4	1.6	1.8	2.0	2.2	2.4	2.6	2.8	3.0	3.2
$\Psi_{s-c,V}$	1.00	1.31	1.66	2.02	2.41	2.83	3.26	3.72	4.19	4.69	5.20	5.72

##### FOR 2 ANCHORS FASTENING

Reduction Factor  $\Psi_{s-c,V}$

Non-cracked concrete

$\frac{c}{c_{min}}$	1.0	1.2	1.4	1.6	1.8	2.0	2.2	2.4	2.6	2.8	3.0	3.2
$\frac{s}{c_{min}}$												
1.0	0.67	0.84	1.03	1.22	1.43	1.65	1.88	2.12	2.36	2.62	2.89	3.16
1.5	0.75	0.93	1.12	1.33	1.54	1.77	2.00	2.25	2.50	2.76	3.03	3.31
2.0	0.83	1.02	1.22	1.43	1.65	1.89	2.12	2.38	2.63	2.90	3.18	3.46
2.5	0.92	1.11	1.32	1.54	1.77	2.00	2.25	2.50	2.77	3.04	3.32	3.61
3.0	1.00	1.20	1.42	1.64	1.88	2.12	2.37	2.63	2.90	3.18	3.46	3.76
3.5		1.30	1.52	1.75	1.99	2.24	2.50	2.76	3.04	3.32	3.61	3.91
4.0			1.62	1.86	2.10	2.36	2.62	2.89	3.17	3.46	3.75	4.05
4.5				1.96	2.21	2.47	2.74	3.02	3.31	3.60	3.90	4.20
5.0					2.33	2.59	2.87	3.15	3.44	3.74	4.04	4.35
5.5						2.71	2.99	3.28	3.57	3.88	4.19	4.50
6.0							2.83	3.11	3.41	3.71	4.02	4.33

##### FOR OTHER CASE OF FASTENINGS

$$\Psi_{s-c,V} = \frac{3c + s_1 + s_2 + s_3 + \dots + s_{n-1}}{3nc_{min}} \cdot \sqrt{\frac{c}{c_{min}}}$$

# MAXIMA 7

## Stainless Steel Anchor Stud (SUS316)



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### Bonded Anchor in Glass Capsule

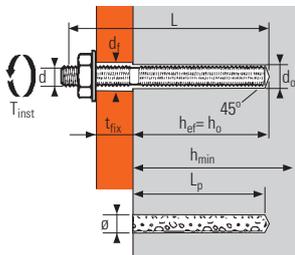
Performance				Material	Installation							

### Technical Data

MAXIMA 7	Anchor depth (mm)	Max thick of fixture (mm)	Drill depth (mm)	Min thick of base material (mm)	Ø Thread (mm)	Ø Drill bit (mm)	Total anchor length (mm)	Max tighten torque (Nm)	Chemset stud code	Ramset power tool code	Drill bit type-size
	$h_{ef}$	$t_{fix}$	$h_o$	$h_{min}$	$d$	$d_o$	$L$	$T_{inst}$			
MAXIMA M8	80	15	80	120	8	10	110	10	CS08110SS	DD527	R3 PLUS-10
MAXIMA M10	90	20	90	130	10	12	130	20	CS10130SS	DD527	R3 PLUS-12
MAXIMA M12	110	25	110	160	12	14	160	30	CS12160SS	DD527	R3 PLUS-14
MAXIMA M16	125	35	125	175	16	18	190	60	CS16190SS	DD543	R3 PLUS-18
MAXIMA M20	170	65	170	220	20	25	260	120	CS20260SS	DD565	R3 MAX-25
MAXIMA M24	210	63	210	270	24	28	300	200	CS24300SS	DD565	R3 MAX-28
MAXIMA M30	280	70	280	340	30	35	380	400	CS30380SS	DD565	R3 MAX-35



ETA Option 7  
n° 03/0008



### MATERIAL

Stud:  
SUS316

Hexagonal nut:  
SUS316

Washer:  
SUS316

### Anchor Mechanical Properties

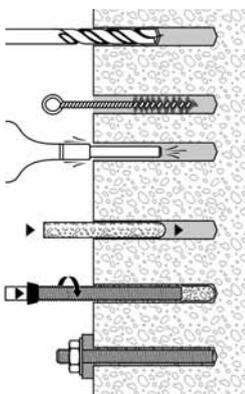
STAINLESS STEEL SUS316	M8	M10	M12	M16	M20	M24	M30
$f_{uk}$ (N/mm <sup>2</sup> ) Min. tensile strength	650	650	650	650	650	650	500
$f_{yk}$ (N/mm <sup>2</sup> ) Yield strength	450	450	450	450	450	450	250
$A_s$ (mm <sup>2</sup> ) Stressed cross-section	36.6	58.0	84.3	157.0	245.0	353.0	522.8
$W_{el}$ (mm <sup>3</sup> ) Elastic section modulus	31.2	62.3	109.2	277.5	540.9	935.5	1,686.0
$M^0_{Rk,s}$ (Nm) Characteristic bending moment	24.3	48.6	85.2	216.5	421.9	729.7	1,011.6
$M$ (Nm) Recommended bending moment	15.7	31.4	55.0	139.6	272.2	364.8	652.6

### Setting Time before applying load

Ambient temperature (°C)

	Dry concrete	Wet concrete
	Waiting time before apply load	Waiting time before apply load
$T \geq 20^\circ\text{C}$	20 min	40 min
$10^\circ\text{C} < T < 20^\circ\text{C}$	30 min	60 min
$0^\circ\text{C} < T < 10^\circ\text{C}$	1 hour	2 hours
$-5^\circ\text{C} < T < 0^\circ\text{C}$	5 hours	10 hours

### INSTALLATION



### Chemical Resistance of the MAXIMA Anchor

Chemical substances	Concentration (%)	Resistance	Chemical substances	Concentration (%)	Resistance
Nitric Acid	< 20	1	Carbon monoxide	100	1
Phosphoric acid	< 10	1	Caustic potash	100	1
Sulphuric acid	$\leq 30$	1	Nitric Acid	20 - 70	2
Ethyl alcohol	$\leq 15$	1	Heptane	100	2
Beer	100	1	Hexane	100	2
Carbon dioxide	100	1	Methanol	$\leq 15$	2
Hydrogen fluoride	$\leq 20$	1	Perchloroethylene	100	2
Ammonia	100	1	Hydrogen peroxide	$\leq 40$	2
Ethylene glycol	100	1	Sulphurous acid	100	2
Washing powder	100	1	Engine petrol w/o benzene	100	2
Cement in suspension saturated solution		1			

1 = High resistance (Anchors could be submerged in these materials)

2 = Medium resistance (Anchors could be temporary submerged due to splash or spill)

# MAXIMA 7

## Stainless Steel Anchor Stud (SUS316)



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### Ultimate Loads ( $N_{Ru,m}$ , $V_{Ru,m}$ ) / Characteristic Loads ( $N_{Rk}$ , $V_{Rk}$ ) in kN

#### TENSILE @ Concrete strength 30 N/mm<sup>2</sup>

Anchor size	M8	M10	M12	M16	M20	M24	M30
$h_{ef}$ (mm)	80	90	110	125	170	210	280
$N_{Ru,m}$ (kN)	25.7	40.7	59.2	102.5	167.8	231.6	327.5
$N_{Rk}$ (kN)	23.8	37.7	54.8	76.9	125.8	173.7	270.7

#### SHEAR @ Concrete strength 30 N/mm<sup>2</sup>

Anchor size	M8	M10	M12	M16	M20	M24	M30
$V_{Ru,m}$ (kN)	15.4	24.4	35.5	66.1	103.2	148.7	169.4
$V_{Rk}$ (kN)	14.3	22.6	32.9	61.2	95.6	137.7	156.8

### Design Loads ( $N_{Rd}$ , $V_{Rd}$ ) for one anchor without edge or spacing influence in kN

$$N_{Rd} = \frac{N_{Rk}}{\gamma_{Mc,N}}$$

$$V_{Rd} = \frac{V_{Rk}}{\gamma_{Ms,V}}$$

#### TENSILE @ Concrete strength 30 N/mm<sup>2</sup>

Anchor size	M8	M10	M12	M16	M20	M24	M30
$h_{ef}$ (mm)	80	90	110	125	170	210	280
$N_{Rd}$ (kN)	15.4	24.3	35.4	42.7	69.9	96.5	150.4

$$\gamma_{Mc,N} = 1.8$$

$$\gamma_{Ms,N} = 1.55 \text{ (steel failure) for M8 to M24}$$

#### SHEAR @ Concrete strength 30 N/mm<sup>2</sup>

Anchor size	M8	M10	M12	M16	M20	M24	M30
$V_{Rd}$ (kN)	9.2	14.6	21.2	39.5	61.6	88.8	78.4

$$\gamma_{Ms,V} = 1.55 \text{ for M8 to M24}$$

$$\gamma_{Ms,V} = 2.00 \text{ for M30}$$

### Recommended Loads ( $N_{rec}$ , $V_{rec}$ ) for one anchor without edge or spacing influence in kN

$$N_{rec} = \frac{N_{Rk}}{\gamma_{Mc,N} \cdot \gamma_F}$$

$$V_{rec} = \frac{V_{Rk}}{\gamma_{Ms,V} \cdot \gamma_F}$$

#### TENSILE @ Concrete strength 30 N/mm<sup>2</sup>

Anchor size	M8	M10	M12	M16	M20	M24	M30
$h_{ef}$ (mm)	80	90	110	125	170	210	280
$N_{rec}$ (kN)	11.0	17.4	25.3	30.5	49.9	68.9	107.4

$$\gamma_F = 1.4$$

$$\gamma_{Mc,N} = 1.8$$

$$\gamma_{Ms,N} = 1.55 \text{ (steel failure) for M8 to M24}$$

#### SHEAR @ Concrete strength 30 N/mm<sup>2</sup>

Anchor size	M8	M10	M12	M16	M20	M24	M30
$V_{rec}$ (kN)	6.6	10.4	15.2	28.2	44.0	63.4	56.0

$$\gamma_F = 1.4$$

$$\gamma_{Ms,V} = 1.55 \text{ for M8 to M24}$$

$$\gamma_{Ms,V} = 2.00 \text{ for M30}$$

steel failure

# MAXIMA 7

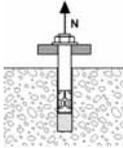
## Stainless Steel Anchor Stud (SUS316)



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### CC-Method

#### TENSILE in kN



Pull-out resistance  
Concrete strength 30 N/mm<sup>2</sup>

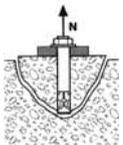
$$N_{Rd,p} = N^0_{Rd,p} \cdot f_B \cdot f_T$$

Design resistance in dry and wet concrete							
Anchor size	M8	M10	M12	M16	M20	M24	M30
$N^0_{Rd,p}$	11.9	20.2	30.8	42.7	69.9	96.5	150.4

Design resistance in flooded concrete							
Anchor size	M8	M10	M12	M16	M20	M24	M30
$N^0_{Rd,p}$	8.5	14.4	22.0	30.5	49.9	68.9	107.4

$$\gamma_{Mc,N} = 1.8$$

$$\gamma_{Mc,N} = 2.52 \text{ (flooded)}$$



Concrete cone resistance for dry (1), wet (2) and flooded (3) concrete

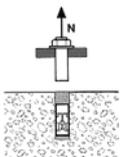
$$N_{Rd,c} = N^0_{Rd,c} \cdot f_B \cdot f_T \cdot \Psi_s \cdot \Psi_{c,N}$$

Design resistance in dry and wet concrete							
Anchor size	M8	M10	M12	M16	M20	M24	M30
$N^0_{Rd,c}$	26.3	31.4	42.5	51.4	81.6	112.0	172.5

Design resistance in flooded concrete							
Anchor size	M8	M10	M12	M16	M20	M24	M30
$N^0_{Rd,c}$	15.7	18.7	25.3	30.6	48.6	66.7	102.6

$$\gamma_{Mc,N} = 1.5$$

$$\gamma_{Mc,N} = 2.52 \text{ (flooded)}$$



Steel resistance

Steel design tensile resistance							
Anchor size	M8	M10	M12	M16	M20	M24	M30
$N_{Rd,s}$	15.4	24.3	35.4	65.9	102.8	148.1	130.7

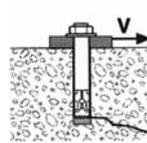
$$\gamma_{Ms,N} = 1.55 \text{ for M8 to M24}$$

$$\gamma_{Ms,N} = 2.00 \text{ for M30}$$

$$N_{Rd} = \min(N_{Rd,p}; N_{Rd,c}; N_{Rd,s})$$

$$\beta N = N_{Sd} / N_{Rd} \leq 1$$

#### SHEAR in kN



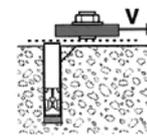
Concrete edge resistance  
Concrete strength 30 N/mm<sup>2</sup>

$$V_{Rd,c} = V^0_{Rd,c} \cdot f_B \cdot f_{\beta,V} \cdot \Psi_{s-c,V}$$

Design concrete edge resistance at a minimum edge distance ( $c_{min}$ )							
Anchor size	M8	M10	M12	M16	M20	M24	M30
$V^0_{Rd,c}$	2.8	3.6	5.3	7.5	13.3	19.7	34.3

$c_{min}$	40	45	55	65	85	105	140
$s_{min}$	40	45	55	65	85	105	140

$$\gamma_{Mc,V} = 1.5$$

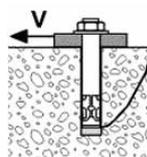


Steel resistance

Steel design shear resistance							
Anchor size	M8	M10	M12	M16	M20	M24	M30
$V_{Rd,s}$	9.2	14.6	21.2	39.5	61.6	88.8	78.4

$$\gamma_{Ms,V} = 1.55 \text{ for M8 to M24}$$

$$\gamma_{Ms,V} = 2.00 \text{ for M30}$$



Concrete pry-out failure  
Concrete Strength 30 N/mm<sup>2</sup>

$$V_{Rd,cp} = V^0_{Rd,cp} \cdot f_B \cdot \Psi_s \cdot \Psi_{c,N}$$

Design pry-out resistance							
Anchor size	M8	M10	M12	M16	M20	M24	M30
$V^0_{Rd,cp}$	23.5	36.7	58.6	88.0	110.0	168.7	205.4

$$\gamma_{Mc,V} = 1.5$$

- (1) for dry hole,  $\gamma_{Mc} = 2.16$  where brush is not use to clean hole
- (2) The concrete in the area of the anchorage is water saturated.
- (3) The concrete is wet, and the is full of water. The resin can be injected without remove water.

$$V_{Rd} = \min(V_{Rd,c}; V_{Rd,s}; V_{Rd,cp})$$

$$\beta V = V_{Sd} / V_{Rd} \leq 1$$

$$\beta N + \beta V \leq 1.2$$

#### $f_B$ INFLUENCE OF CONCRETE

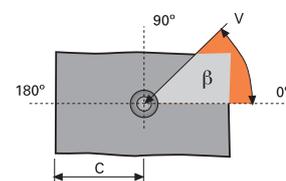
Concrete Grade	$f_B$	Concrete Grade	$f_B$
C16/20	0.81	C35/45	1.21
C20/25	0.90	C40/50	1.28
C25/30	1.00	C45/55	1.34
C30/37	1.10	C50/60	1.40

#### $f_T$ INFLUENCE OF EMBEDMENT DEPTH

$$f_T = \frac{h_{act}}{h_{ef}} \text{ where: } h_{ef} \leq h_{act} \leq 2h_{ef}$$

#### $f_{\beta,V}$ INFLUENCE OF SHEAR LOADING DIRECTION

Angle $\beta$ [°]	$f_{\beta,V}$
0~50	1.0
60	1.1
70	1.2
80	1.5
90~180	2.0



# MAXIMA 7

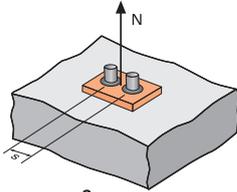
## Stainless Steel Anchor Stud (SUS316)



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### CC-Method

#### $\Psi_s$ INFLUENCE OF SPACING FOR CONCRETE CONE RESISTANCE IN TENSILE LOAD



$$\Psi_s = 0.5 + \frac{s}{4h_{ef}}$$

$$s_{min} < s < s_{cr,N}$$

$$s_{min} = 0.5h_{ef}$$

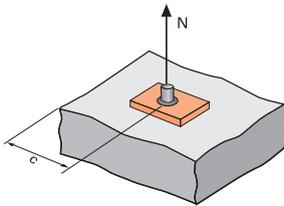
$$s_{cr,N} = 2h_{ef}$$

$\Psi_s$  must be used for each spacing influenced the anchors group

Spacing, s	Reduction Factor $\Psi_s$ Non-cracked concrete			
	M8	M10	M12	M16
40	0.63			
45	0.64	0.63		
55	0.67	0.65	0.63	
65	0.70	0.68	0.65	0.63
85	0.77	0.74	0.69	0.67
105	0.83	0.79	0.74	0.71
140	0.94	0.89	0.82	0.78
160	1.00	0.94	0.86	0.82
180		1.00	0.91	0.86
220			1.00	0.94
250				1.00

Spacing, s	Reduction Factor $\Psi_s$ Non-cracked concrete		
	M20	M24	M30
85	0.63		
105	0.65	0.63	
140	0.71	0.67	0.63
160	0.74	0.69	0.64
180	0.76	0.71	0.66
220	0.82	0.76	0.70
250	0.87	0.80	0.72
300	0.94	0.86	0.77
340	1.00	0.90	0.80
370		0.94	0.83
450		1.00	0.90
560			1.00

#### $\Psi_{c,N}$ INFLUENCE OF EDGE FOR CONCRETE CONE RESISTANCE IN TENSILE LOAD



$$\Psi_{c,N} = 0.275 + 0.725 \cdot \frac{c}{h_{ef}}$$

$$c_{min} < c < c_{cr,N}$$

$$c_{min} = 0.5h_{ef}$$

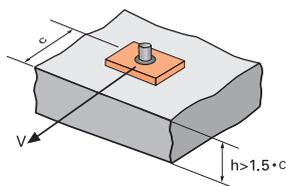
$$c_{cr,N} = h_{ef}$$

$\Psi_{c,N}$  must be used for each distance influenced the anchors group

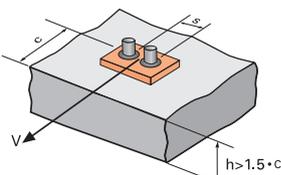
Edge, c	Reduction Factor $\Psi_{c,N}$ Non-cracked concrete			
	M8	M10	M12	M16
40	0.63			
45	0.68	0.63		
55	0.77	0.71	0.63	
65	0.86	0.79	0.70	0.66
80	1.00	0.91	0.80	0.73
90		1.00	0.86	0.79
110			1.00	0.91
125				1.00

Edge, c	Reduction Factor $\Psi_{c,N}$ Non-cracked concrete		
	M20	M24	M30
85	0.63		
105	0.72	0.63	
120	0.78	0.68	
140	0.87	0.75	0.63
170	1.00	0.86	0.71
210		1.00	0.81
250			0.92
280			1.00

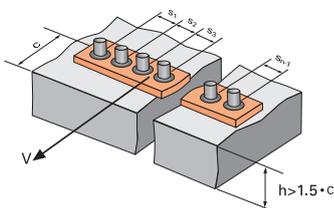
#### $\Psi_{s-c,V}$ INFLUENCED OF SPACING AND EDGE DISTANCE FOR CONCRETE EDGE RESISTANCE IN SHEAR LOAD



$$\Psi_{s-c,V} = \frac{c}{c_{min}} \cdot \sqrt{\frac{c}{c_{min}}}$$



$$\Psi_{s-c,V} = \frac{3c + s}{6c_{min}} \cdot \sqrt{\frac{c}{c_{min}}}$$



##### FOR SINGLE ANCHOR FASTENING

$\frac{c}{c_{min}}$	Reduction Factor $\Psi_{s-c,V}$ Non-cracked concrete											
	1.0	1.2	1.4	1.6	1.8	2.0	2.2	2.4	2.6	2.8	3.0	3.2
$\Psi_{s-c,V}$	1.00	1.31	1.66	2.02	2.41	2.83	3.26	3.72	4.19	4.69	5.20	5.72

##### FOR 2 ANCHORS FASTENING

$\frac{s}{c_{min}}$	Reduction Factor $\Psi_{s-c,V}$ Non-cracked concrete												
	$\frac{c}{c_{min}}$	1.0	1.2	1.4	1.6	1.8	2.0	2.2	2.4	2.6	2.8	3.0	3.2
1.0	0.67	0.84	1.03	1.22	1.43	1.65	1.88	2.12	2.36	2.62	2.89	3.16	
1.5	0.75	0.93	1.12	1.33	1.54	1.77	2.00	2.25	2.50	2.76	3.03	3.31	
2.0	0.83	1.02	1.22	1.43	1.65	1.89	2.12	2.38	2.63	2.90	3.18	3.46	
2.5	0.92	1.11	1.32	1.54	1.77	2.00	2.25	2.50	2.77	3.04	3.32	3.61	
3.0	1.00	1.20	1.42	1.64	1.88	2.12	2.37	2.63	2.90	3.18	3.46	3.76	
3.5		1.30	1.52	1.75	1.99	2.24	2.50	2.76	3.04	3.32	3.61	3.91	
4.0			1.62	1.86	2.10	2.36	2.62	2.89	3.17	3.46	3.75	4.05	
4.5				1.96	2.21	2.47	2.74	3.02	3.31	3.60	3.90	4.20	
5.0					2.33	2.59	2.87	3.15	3.44	3.74	4.04	4.35	
5.5						2.71	2.99	3.28	3.57	3.88	4.19	4.50	
6.0							2.83	3.11	3.41	3.71	4.02	4.33	4.65

##### FOR OTHER CASE OF FASTENINGS

$$\Psi_{s-c,V} = \frac{3c + s_1 + s_2 + s_3 + \dots + s_{n-1}}{3nc_{min}} \cdot \sqrt{\frac{c}{c_{min}}}$$